Abstract

In recent years, turbine inlet temperature becomes higher and higher to grow up the power of gas turbine engines. The hot section parts, such as combustor and turbine, are generally designed as cooling structures which were made of heat resistant metals. However, some organizations research and develop the ceramics parts as next generation materials instead of heat resistant steels[1][2].

The purpose of this research is thrust growth of jet engine without increasing the outer diameter dimensions, so turbine inlet temperature must be increased. For that higher turbine inlet temperature, turbine nozzle is air cooled metal airfoils and turbine blade is ceramic turbine wheel with blade since air cooled metal blades is too complicated and expensive.

This paper describes the current achievement of the research of the ceramic turbine jet engine initiated in 1997.

2 Jet Engine Configuration

The type of this jet engine is most simple single spool turbo jet engine. Figure 1 shows the ceramic turbine jet engine configuration. The main parts consist of combined compressor of single axial type and single centrifugal type, annular type combustor with spray type and single axial turbine, and ceramic turbine wheel is adopted. Turbine nozzle material is heat resistant steel, so that has air cooled airfoils with film cooling holes and so on.
3 Design of Ceramic Turbine

The main parameter of ceramic turbine is shown in Table 1. Silicon nitride ($\text{Si}_3\text{N}_4$) was adopted as design material because of its higher strength in high temperature.

3.1 Material Test

Various material tests were carried out to get the basic material data for the design. At first, test pieces were cut out from the wheel in Fig. 2 and 4 points bending test was carried out. The cut out positions of these test pieces were bore position (near inner diameter of wheel) and neck position (most thin position of wheel). And the test pieces of neck position were two kind of surface conditions, as machined and as fired. Because the wheel surface sections as machined must be reduced for the cost down and the data of test piece as fired must be needed.

Table 1 Main parameter of ceramic turbine

<table>
<thead>
<tr>
<th>Item</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Material</td>
<td>$\text{Si}_3\text{N}_4$</td>
</tr>
<tr>
<td>Tip diameter</td>
<td>$\phi$ 218mm</td>
</tr>
<tr>
<td>Rotational speed</td>
<td>490m/s(Tip speed)</td>
</tr>
<tr>
<td>Inlet temperature</td>
<td>1,100°C</td>
</tr>
<tr>
<td>Inlet Pressure</td>
<td>1.030kPa</td>
</tr>
<tr>
<td>Power</td>
<td>1,900kW</td>
</tr>
</tbody>
</table>

Fig. 3 Bending test results (room temperature)

Fig. 4 Bending test results (1100°C)
From these results, the new design curve of ceramic turbine was decided as follows, the surface strength was as same as that of test piece as fired and the inner strength was as same as that of test piece as machined.

In order to confirm the failing rotational speed, rotational test for the ceramic turbine wheel was carried out under the room temperature condition. Figure 5 shows the results of rotational test. It is seen from Fig. 5 that the failure probability curve based on design has the sufficient margin to the test results.

3.2 Design of Connected Section

The subject of application of ceramic turbine is the way to connect the ceramic turbine and rotational shaft. Thermal expansion ratio of ceramic is lower than that of metal alloys and so the difference of thermal expansion between a ceramic part and a metal alloy part is occurred. Ceramic is brittle material and weak in the peak stress by the stress concentration. Therefore, it is difficult that ceramic turbine is directly fixed with the rotational shaft. The metal flange with low thermal expansion is fixed with the ceramic turbine by shrinkage fit method, and ceramic turbine is fixed with rotational shaft by using that flange. Figure 6 shows the structure of connection of ceramic turbine and rotational shaft in the test engine.

The tight force of this shrinkage fit section was confirmed by the preliminary simple model test. The outline of the simple model test is shown in Fig. 7. The metal flange is fixed with the ceramic test piece which has the same dimension of shrinkage fit section as the ceramic turbine by shrinkage fit method. Then 10 same models were produced and the constrain force dispersion was confirmed by measuring the each constrain force. The method of this test was followings; heated up to 500℃ more than the used temperature, and fixed the metal flange, and...
added the load against ceramic. The load was added three times against the same model and the load to pull out ceramic was measured. The test results are shown in Fig. 8. The structural reliability of the shrinkage fit section is confirmed by the simple model test under the high temperature condition (500°C). Furthermore, the standard design load corresponding to -3 $\sigma$ was estimated by the test results.

4 Proof Test of Ceramic Turbine

As the characteristics of ceramic, ceramic has a tendency to increasing the defects in proportion to its volume, and it has possibility to be broken by the small defect which is not found by Non Destructive Inspection (NDI), since ceramic is fragile material. Therefore, for proof of ceramic products, it is indispensable to screening by adding the load to ceramic turbine. This ceramic turbine is rotational part, so basic proof test is rotational test. In addition, for the proof test of blades, blade bending test was carried out. Figure 9 shows the proof test setup.

5 Engine Test

Ceramic turbine manufactured with using these design concepts was applied to the engine test. Engine test is started from Sea Level Static (SLS) condition test, and test condition gradually stepped up. Finally engine test was carried out under the condition of compressed

Fig. 8 Results of simple model test

Fig. 9 Proof test setup

Fig. 10 Ceramic turbine in the engine
RESEARCH ON APPLICATION OF CERAMIC TURBINE TO JET ENGINE

inlet air as the flight mach number. Test engine configuration was two types, normal type jet engine and onrotor type engine with the slip ring to measure the temperature on shrinkage fit section of ceramic turbine in the engine operation. The ceramic turbine setup in the engine and the engine test (under flight condition) setup are shown in Figs 10 and 11, respectively. Schematic of the onrotor type engine with slipring is shown in Fig. 12.

Figure 13 shows the results of engine test. The test results indicate the ceramic turbine is capable of operating under the condition of fast starting to full speed. Table 2 shows the temperature of shrinkage fit section in operating the engine. It is seen from Table 2 that the measured temperature and the estimated temperature under flight condition are less than the allowable temperature respectively.

6 Conclusions

In this study, the ceramic turbine is applied in the aircraft gas turbine engine. The structural reliability of ceramic turbine component in the aircraft gas turbine engine has been confirmed by the engine test with the engine performance based on design. The result of this study has got a prospect of application of ceramic turbine to jet engine.

In the future study, higher structural reliability of the ceramic turbine is needed to the actual use of the ceramic turbine jet engines.

References